

- Introduction
- Amplificateur différentiel
- Caractéristiques Grands signaux
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Electronique II

Good morning everyone. We practically arrive to the end of the analysis of all the basic structures. So in this video, we will learn what is called the differential amplifier. So with this last structure, we are going to make a type of amplifier that is a bit special, it's a bit similar to the common transmitter, but you will see right away that there is a fundamental difference compared to the common transmitter. And I will end in this series this week by the Darlington setup analysis and then I will resume everything we saw since the beginning of the study of transistors up to all the structures which we analyzed just to refresh the mind of those who follow this course. And I'll conclude with a treatment of a complete exercise which allowing you to see how is it used or how it is synthesized using different basic analog structures that we have traveled so far. So it is a crucial week because it will summarize all of what we saw from the beginning.

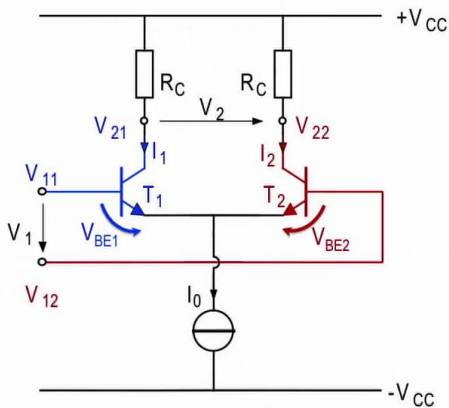
Notes

Summary



0m 05s

Amplificateur différentiel, principe



$$A_v = -g_m R_C$$

$$I_0 = I_1 + I_2 \quad (I_1 - I_2 = I_0/2 \text{ si } V_1 = 0)$$

$$V_1 = V_{11} - V_{12} = V_{BE1} - V_{BE2}$$

Electronique II

A differential amplifier, that is drawn here, compared to a common emitter amplifier, which I'll draw next so if you take our famous common emitter, where we had a transistor then we arranged in a small pattern signals, to connect its emitter to a fixed potential. So look, it's a fixed potential. They put a RC load and they brought a signal, in a manner to give an increase here and called this V1, and called this V2. If I compare this to that, I see there, the voltage V1 and the voltage V2 are both compared to a fixed potential. And it is a potential that we have a priori imposed. So it's a potential that can be grounded, someone has imposed, or a DC voltage. I will not go into details on how it is created because we saw it in long and wide. When you see the variation of the voltage V2 relative to this fixed potential, brought for example to V1 finally, this potential that is the same, well, this generates a current passing in RC etc. etc. I will like to compare this to this, just remember that the gain that was found, this is a gain which is $-g_m \times R_C$ and g_m corresponds to a polarized current divided by U_T . I come to this setup. Look there. Instead of one transistor, I put two.

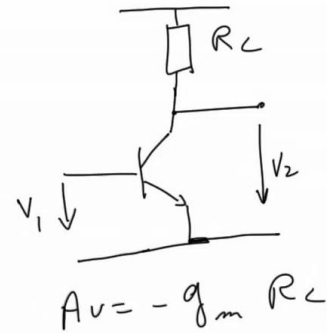
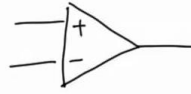
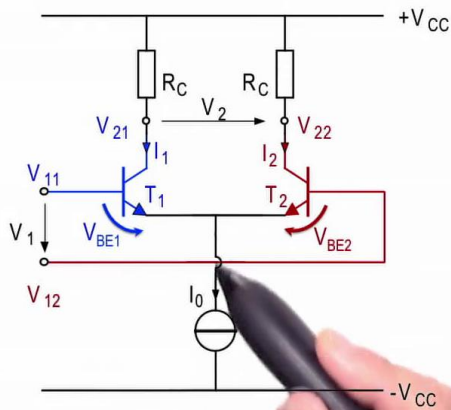
Notes

Summary



1m 09s

Amplificateur différentiel, principe



$$I_0 = I_1 + I_2 \quad (I_1 - I_2 = I_0/2 \text{ si } V_1 = 0)$$

$$V_1 = V_{11} - V_{12} = V_{BE1} - V_{BE2}$$

Electronique II

Both transistors are connected by their transmitters and the two bases constitute the input to this setup and the two terminals that you see, V11, V12 are generally, these two terminals that, quite often, when you take an operational amplifier you were told that there is an input (+) and an input (-) and in it is an integrated circuit, and this circuit represents a positive-negative input that are in reality these two potentials V11 and V12 and they say to you here, there is a differential voltage and often there is such a gain there, that this gain is terribly great to make these two tensions close to each other. They say in an ideal amp, the gain is infinite and $V(+) = V(-)$. So in reality, there is a setup like this placed at the input of an setup of the type of integrated circuit which is the operational amplifier. The comparison to the common transmitter, I return to this point, it's that an issuer that is in between, it floats. Look, we put a power source, this current source, in terms of DC, It could endure any DC potential. So you can apply here any voltage that would float between the supply rails, between (+ VCC) and (-VCC).

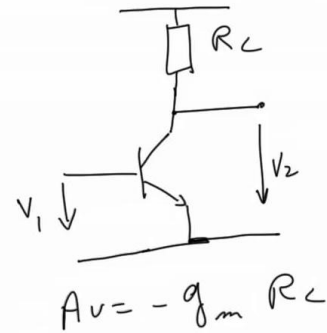
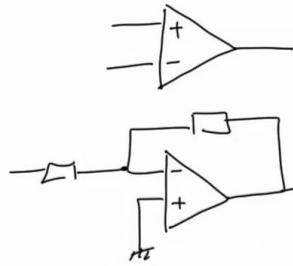
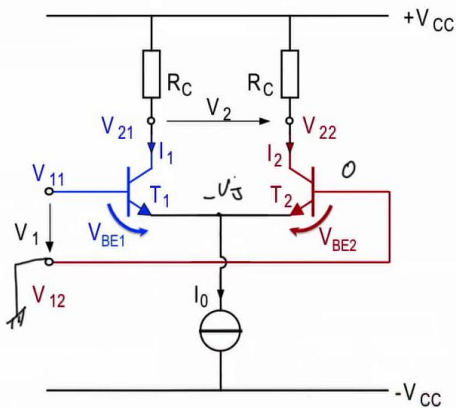
Notes

Summary



2m 41s

Amplificateur différentiel, principe



$$I_0 = I_1 + I_2 \quad (I_1 - I_2 = I_0/2 \text{ si } V_1 = 0)$$

$$V_1 = V_{11} - V_{12} = V_{BE1} - V_{BE2}$$

Electronique II

So it is a potential which is quite arbitrary, which is imposed by the person who is doing the setup. So if you take an operational amplifier, and I will take, ie, amplifier with a potential, the (+) to ground against a feedback through resistors, and you will see that one has the impression that imposes a potential 0 here And they say, "Here is the entrance to the other side." So it's like someone is taking the (+) and impose it on one of these two inputs, So if you plug it here, and you say: this setup is inside, we will reason on this reflection, they will say: there, one has a given potential data, good, we will go to 0 V, there, I have a voltage drop, If the transistor conducts on the order of U_j to DC. So the analysis brings me back quickly that this potential will be stabilize to $-U_j$. So again, I meet the fact that the transmitter of this transistor is found at a fixed potential imposed by someone who as connected from outside a ground. So if the person would come and put a voltage source here well, this voltage source would require a different voltage on the dropping basis of U_j , bring back the transmitter to another value DC.

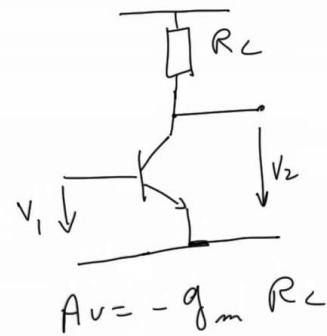
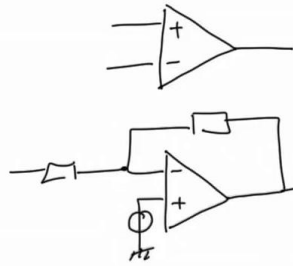
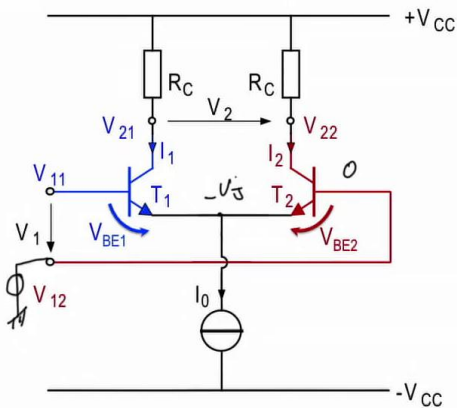
Notes

Summary



4m 04s

Amplificateur différentiel, principe



$$I_0 = I_1 + I_2 \quad (I_1 - I_2 = I_0/2 \text{ si } V_1 = 0)$$

$$V_1 = V_{11} - V_{12} = V_{BE1} - V_{BE2}$$

Electronique II

so basically, we are saying that transmitters are virtually at a stable potential, So we have a DC potential imposed by what would have imposed on the base. when I say all this, to show that we dont have to define it, the potential that had been set and they brought back in a potential imposed by someone, here, it is imposed by anyone that would use this setup, and the setup, alone will adapt and will bring back a polarization to that node.

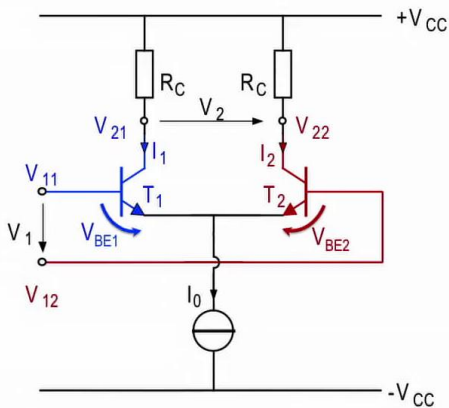
Notes

Summary



5m 32s

Amplificateur différentiel, principe



$$I_0 = I_1 + I_2 \quad (I_1 - I_2 = I_0/2 \text{ si } V_1 = 0)$$

$$V_1 = V_{11} - V_{12} = V_{BE1} - V_{BE2}$$

Electronique II

Then I'll erase all that is written above, and we will begin to analyze with the data which are absolutely linked to a very basic analysis from what I see in this diagram. First, I see that I have a voltage which is located between the base of two transistors and this voltage one, takes into consideration, if I say that, it's V_1 , that too is V_1 , it goes like this, and then, it gives me V_1 . So I can easily write V_1 is $V_{11} - V_{12}$ which is nothing else than $V_{BE1} - V_{BE2}$. Therefore, the input voltage, it takes two junction voltages, but one in opposition to each other. Now I look at what will happen with the currents, I take the two currents I_1 and I_2 , I pass them into 2 transistors I sum both of them in this node there, and I said: I_0 is always equal to the sum of these two. So I impose the fact that there is a current source which is always the sum of the two currents. So let's do an analysis of what we just saw. I re-clear again my arrow and we will analyze it. We will finally say if I impose a common mode here, as just now, we put it to ground, it can be any voltage, if you take a common mode, that is to say that this potential is fixed, and you begin to increase V_1 , that means it's V_{BE1} which will increase, and V_{BE2} that will decrease of the same amount.

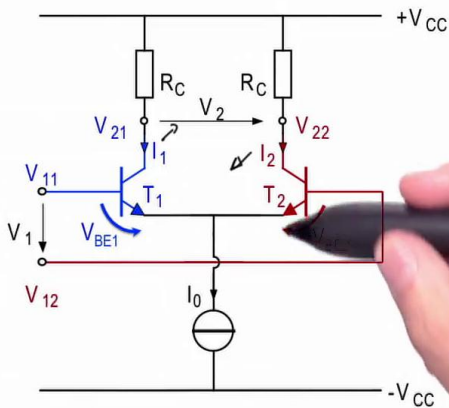
Notes

Summary



6m 07s

Amplificateur différentiel, principe



$$I_0 = I_1 + I_2 \quad (I_1 - I_2 = I_0/2 \text{ si } V_1 = 0)$$

$$V_1 = V_{11} - V_{12} = V_{BE1} - V_{BE2}$$

Electronique II

So any change that I see on V_{BE1} , it is brought back on V_{BE2} and one is in phase opposition compared to other, therefore it increases on one side and it lower on the other side. What will happen with the currents, It's exactly the same thing. When you increase V_{BE1} , you will increase the I_1 current and what happens on the other side, you lower V_{BE2} , therefore, you will reduce the current I_2 . So the two currents will also move in the opposite direction one against another of the same quantity which is shared between 2 transistors. So the one who has understood this, he understood that we have practically a swing with a pivot and this pivot is located around this point and we will rotate it, we will go up or down, what I gain on one side I'll lose it on the other side either from excitement at the input that compared to this current which passing in both branches. Who says current that passes in the two branches, would also say voltage V_2 . Why? Because this current one, it's converted to a voltage through the resistance R_C , it is also converted into a voltage through the resistance R_C and if R_C and R_C are the same, so when the tension rises on one side, it go down on that side there, and vice versa.

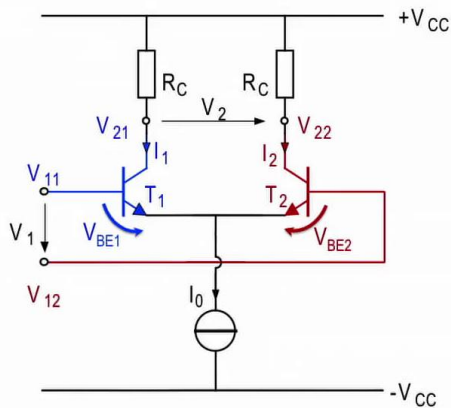
Notes

Summary



7m 38s

Amplificateur différentiel, principe



$$I_1 = I_S \cdot e^{\frac{V_{BE1}}{U_T}}$$

$$I_2 = I_S \cdot e^{\frac{V_{BE2}}{U_T}}$$

$$V_{BE1} = U_T \ln \frac{I_1}{I_S}$$

$$V_{BE2} = U_T \ln \frac{I_2}{I_S}$$

$$V_1 = V_{BE1} - V_{BE2} = U_T \ln \frac{I_1}{I_2} = U_T \ln \frac{\frac{I_1}{I_0}}{\frac{I_2}{I_0}} = U_T \ln \frac{I_1}{I_2}$$

$$I_0 = I_1 + I_2 \quad (I_1 - I_2 = I_0/2 \text{ si } V_1 = 0)$$

$$V_1 = V_{11} - V_{12} = V_{BE1} - V_{BE2}$$

$$I_1 = \frac{I_0}{2} \left[1 + \tanh \left(\frac{V_1}{2U_T} \right) \right],$$

$$I_2 = \frac{I_0}{2} \left[1 - \tanh \left(\frac{V_1}{2U_T} \right) \right]$$

Electronique II

So we will see on the output a differential voltage, if we look between V21 and V22, as we can watch between V22 and V21, - Is it a story of terminal, so we'll see this potential swinging like a swing. You can imagine that when it increases to one side, it go down on the other, and the same of either side, well we control it by the input voltage. It's called the differential pair. I'll take this structure and I will analyze to extract from it an amplifier. I take the diagram of my differential pair. The findings that we have just made here, that is to say it has been said that the sum of voltages V1, it's VBE1 - VBE2, which as noted there and the current flowing I0, it is all the time the sum of blue current and red current, I1+I2 and at rest, when V11 = V12 equal to any voltage wich floating between (-VCC) and (+ VCC) well, you'll fall, on a voltage which is the same on both, so VBE1 = VBE2 and at that time, your current I0 is divided into two and you will have I1 = I0/2 I2 = I0/2 And that's what I've noted here. that's if you have I1 = I2, then there is a mistake is I1 = I2 = I0/2 when the voltage V1 = 0.

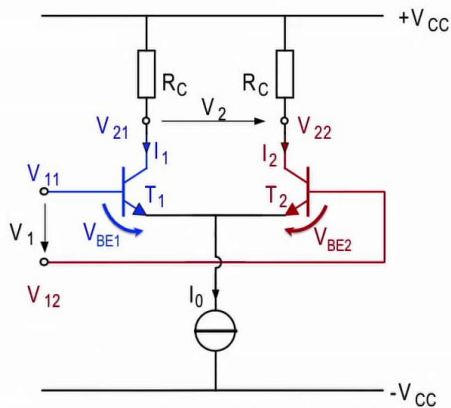
Notes

Summary



8m 54s

Amplificateur différentiel, principe



$$I_1 = I_S \cdot e^{\frac{V_{BE1}}{U_T}}$$

$$V_{BE1} = U_T \ln \frac{I_1}{I_S}$$

$$I_2 = I_S \cdot e^{\frac{V_{BE2}}{U_T}}$$

$$V_{BE2} = U_T \ln \frac{I_2}{I_S}$$

$$V_1 = V_{BE1} - V_{BE2} = U_T \ln \frac{I_1}{I_2} = U_T \ln \frac{\frac{I_1}{I_0}}{1 - \frac{I_1}{I_0}} = U_T \ln \frac{\frac{I_2}{I_0}}{1 - \frac{I_2}{I_0}}$$

$$I_0 = I_1 + I_2 \quad (I_1 - I_2 = I_0/2 \text{ si } V_1 = 0)$$

$$V_1 = V_{11} - V_{12} = V_{BE1} - V_{BE2}$$

$$I_1 = \frac{I_0}{2} \left[1 + \tanh \left(\frac{V_1}{2U_T} \right) \right],$$

$$I_2 = \frac{I_0}{2} \left[1 - \tanh \left(\frac{V_1}{2U_T} \right) \right]$$

Electronique II

I take the transistors laws, each of these transistors is governed by the famous exponential law which would say that the current I_1 is proportional to the control voltage V_{BE1} through this exponential. Same for I_2 . So I will write both laws. I express V_{BE1} therefore, it is logarithm I_1/I_S multiplied by U_T . Same for V_{BE2} . All this, I apply what I see there. I say at the entrance, caution V_{B1} , or rather V_1 , it is the difference of $V_{BE1} - V_{BE2}$ which brings me to simplify this because that is a ratio of I_1/I_2 because I_S is simplified, I replace I_1 by its value because I know that the relation between I_1 and I_2 , it's the complement to this I_0 , and it will give me a relationship between V_1 and I_1 or V_1 and I_2 and I say $I_1 = f(V_1)$. So I take you back to the mathematics courses to see that when I have that kind of relationship, it is called "hyperbolic tangent" and the hyperbolic tangent of $V_1 / 2U_T$, plus 1, multiplied by $I_0 / 2$, is nothing other than the current you order. It is a non-linear law. And there again, it is the expression I_2 which is of the same nature, there is a (-) here and a (+) here and there are I_1 and I_2 expressed. then I'll take these two relations and I'll go and draw that expression and see the plotted relationship between I_1 , I_2 and V_1 . So, I recall that V_1 , it's the differential input voltage.

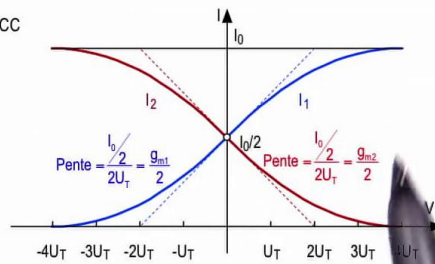
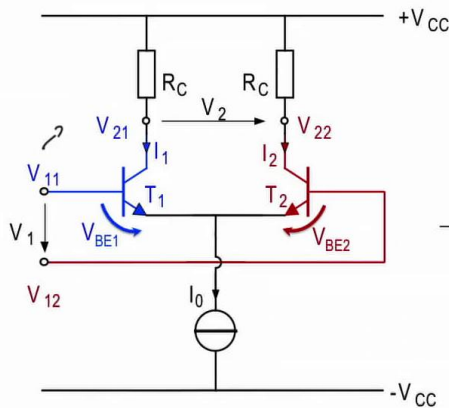
Notes

Summary



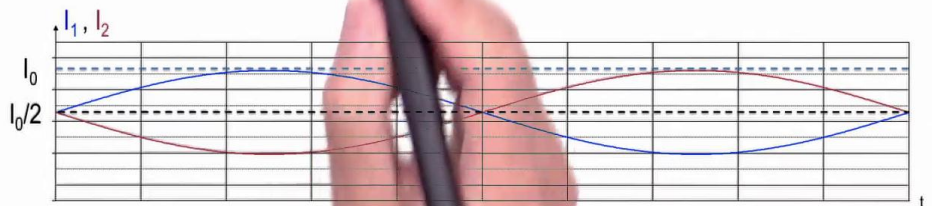
10m 30s

Caractéristiques grands signaux



$$I_1 = \frac{I_0}{2} \left[1 + \tanh\left(\frac{V_1}{2U_T}\right) \right],$$

$$I_2 = \frac{I_0}{2} \left[1 - \tanh\left(\frac{V_1}{2U_T}\right) \right]$$



Electronique II

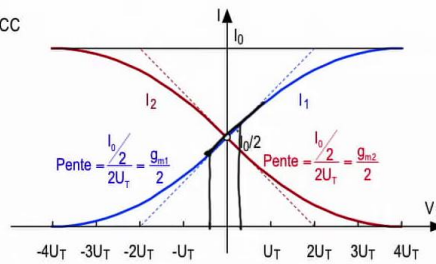
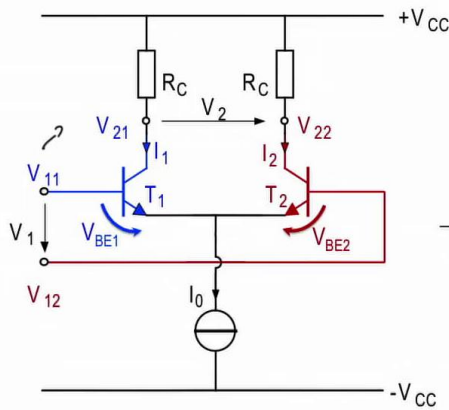
I take I_1 and I_2 and I draw them here. I see indeed if $V_{11} = V_{12}$, equal to a given potential, Well, there $I_0 / 2$ Well, therefore when $V_1 = 0$, so when this was bypassed like that, well, you will end up in that point. When $V_1 = 0$, you find $I_0/2$ the current $I_1 = I_2$. And it's the only one point where the two currents are the same. Because if you start increase V_1 , what's going to happen, if V_1 increases, the V_{BE1} voltage increases, I_1 will increase, And you end up with this current that will increase according to that law. So I_1 will be managed by V_1 and given what is increasing on one side is decreasing from the other side, the other current would follow the same law but in the opposite direction when the current in the blue transistor increases, the other decreases to the same quantity. So the one we add to one side, is subtracted from the other side because the sum of the two is always equal to a constant. so we see that there is a law which describes V_1 , or rather $I = f(V_1)$ sorry $I_1 = f(V_1)$ and $I_2 = f(V_1)$ that is, thereof, the other is red color.

Notes

Summary

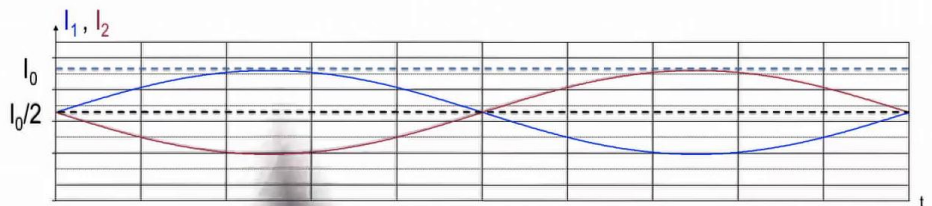


Caractéristiques grands signaux



$$I_1 = \frac{I_0}{2} \left[1 + \tanh\left(\frac{V_1}{2U_T}\right) \right],$$

$$I_2 = \frac{I_0}{2} \left[1 - \tanh\left(\frac{V_1}{2U_T}\right) \right]$$



Electronique II

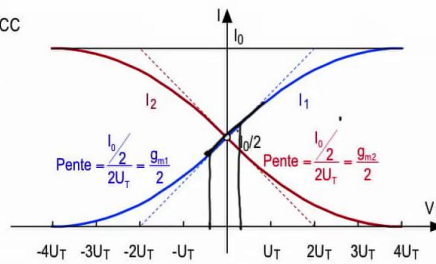
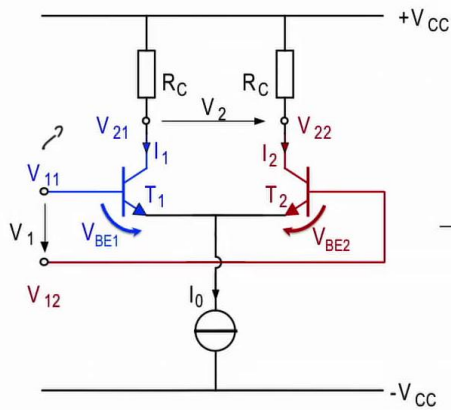
There, what is very interesting is that I find what I'm looking all the time, it is a transconductance me, I wanted to create a structure as the normal transistor where I take a proportion of variation on my curve therefore in this case here, it is the blue line or the red line or both at the same time and I say: finally, the transconductance, is that I'm taking a tension V_1 , I'll vary and I expect that I see a current that follows, What I see here? when I increase V_1 , the current increases and I drops, it is a transconductance but I have it on both sides. So I have two transconductances, I have two currents that follow each other and it is a voltage-current conversion and that current-voltage conversion there is a zone which is fairly linear this is the one I presented as a slope of the tangent around the origin you see with the features blue or red, which are nothing else that the derivative of that law one that will give me the slope of the tangent when I have the current $I_1 = I_2 = I_0/2$ and if I replace this relationship, therefore, I seek the value of the slope analytically the dI / dV_1 when $V_1 = 0$, I come across this relationship $(I_0/2) / 2U_T$. So this is $I_0 / 4U_T$.

Notes

Summary

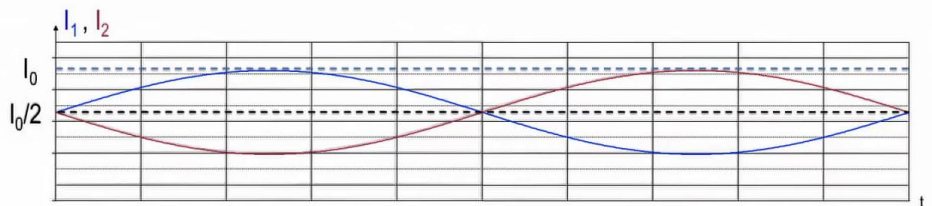


Caractéristiques grands signaux



$$I_1 = \frac{I_0}{2} \left[1 + \tanh\left(\frac{V_1}{2U_T}\right) \right],$$

$$I_2 = \frac{I_0}{2} \left[1 - \tanh\left(\frac{V_1}{2U_T}\right) \right]$$



Electronique II

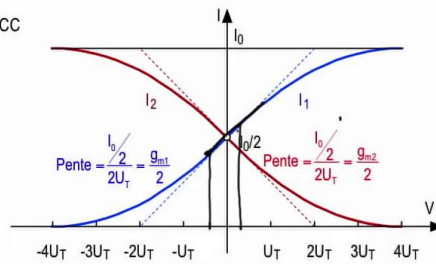
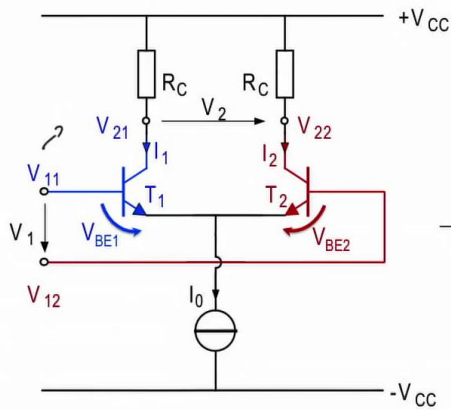
When I tell you to rest, when the voltage $V_{11} = V_{12}$, each of the transistors is driven by the half of this current. So, at rest, I have a current $I_0/2$ and $I_0/2$. So you may well say: the g_{m2} of this transistor that, the g_{m2} of the transistor this is nothing else than the bias current therethrough, divided by U_T . So then this slope is the transconductance of the transistor, $g_{m2}/2$ and that one it's $g_{m1}/2$. So I see here a slope and a slope there, which are nothing other than the transconductance of each of these two transistors. There, in additional, I have traced the variation of the current function on the time when we applying a sinusoidal voltage at the input and when a current increases, the other decreases and when all the current source is deviated in a transistor, it will reach I_0 and when all the current is deviated in the other, it will reach I_0 in the red transistor. So we have a swing where when one hits the ground, we have these swings where there is all the current that switched from one side or the other, well, we've saturated the system. So, we saturate in current because we lost all the current source. since lost all power source. Caution!

Notes

Summary

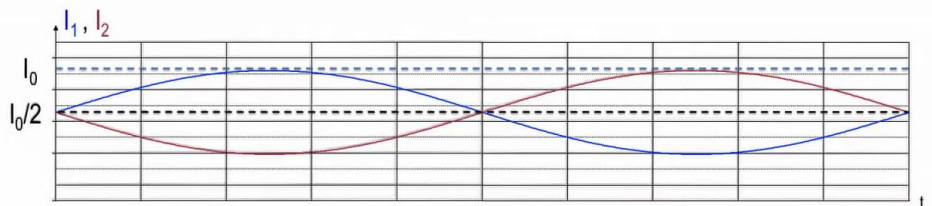


Caractéristiques grands signaux



$$I_1 = \frac{I_0}{2} \left[1 + \tanh\left(\frac{V_1}{2U_T}\right) \right],$$

$$I_2 = \frac{I_0}{2} \left[1 - \tanh\left(\frac{V_1}{2U_T}\right) \right]$$



Electronique II

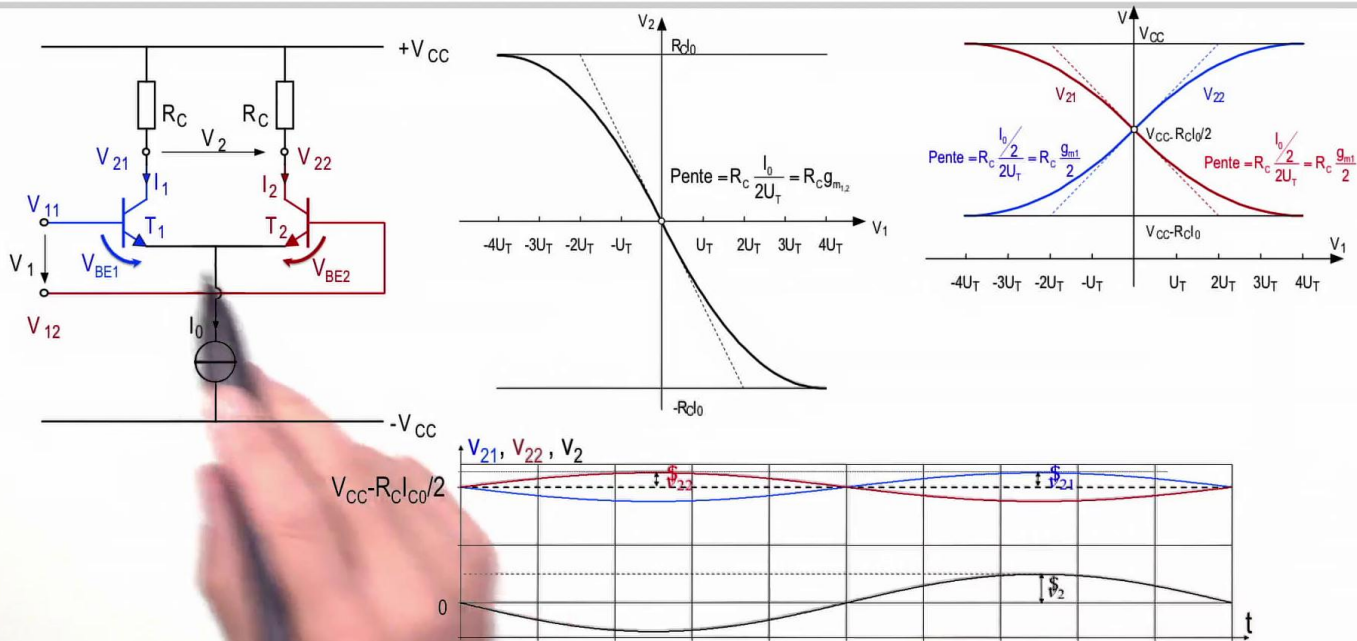
Here I'm not talking about transistor saturation because your transistor when it saturates, is when this voltage is then $U_C = 0$, I'm talking about the saturation of the differential pair whole. It means that all power has already shifted to one side or the other. So we find the same thing you would find with a transistor with that story of transconductance.

Notes

Summary



Caractéristiques grands signaux



Electronique II

We will take now the same explanation but instead of talking about current, we will talk about tension. So instead of saying that the current I_1 and the current I_2 , when one increases, the other will decrease, I will pass currents through a resistance. You remember that resistance, is the element that I use to convert a current into voltage, and I am interested in the change in voltage the terminals of the load because in a pattern small signals, even this tension one will become an short-circuit to the ground so, I'm interested to what is happening with the RC resistance and I am interested in the voltage V_{22} , either compared to the potential one, or relative to another DC potential, since it is a short-circuit in a AC pattern. So if I convert my current into a voltage, and I absolutely expect to see the same characteristic, the same aspect of my curve, I discovered in a short while for the current converted in voltage, because it is through a resistance it would become a voltage V_{22} and V_{21} and these two voltages will exactly follow the same pace that the currents.

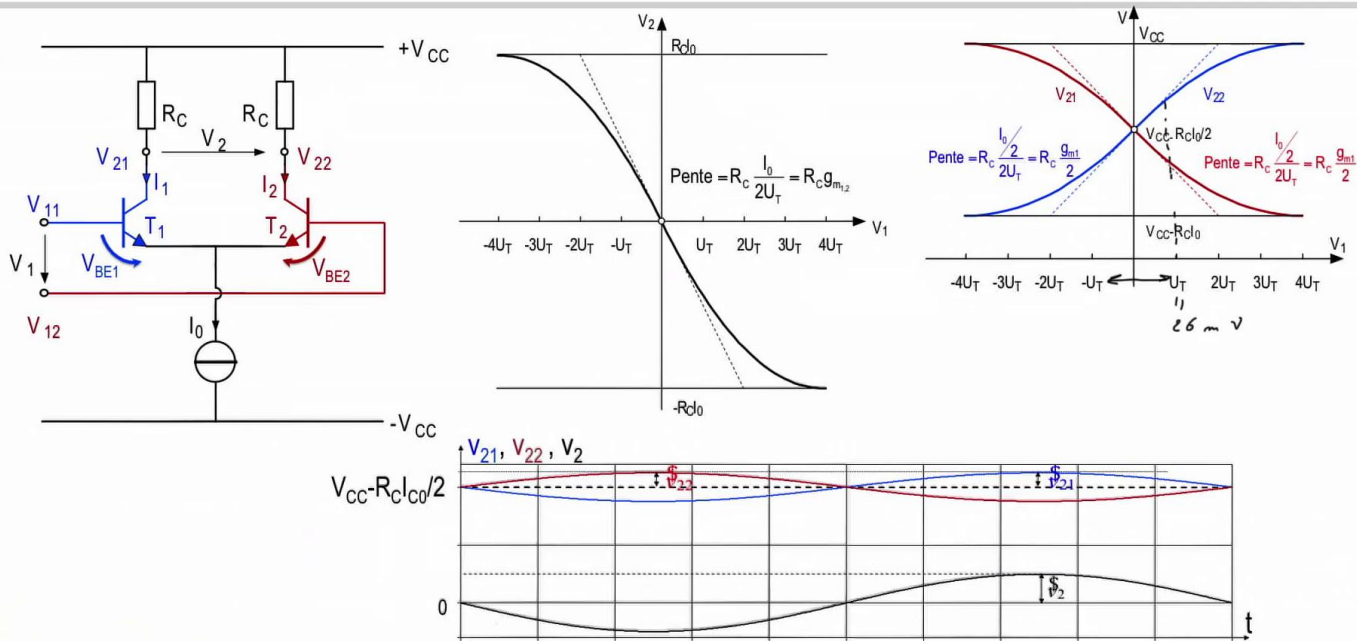
Notes

Summary



16m 51s

Caractéristiques grands signaux



Electronique II

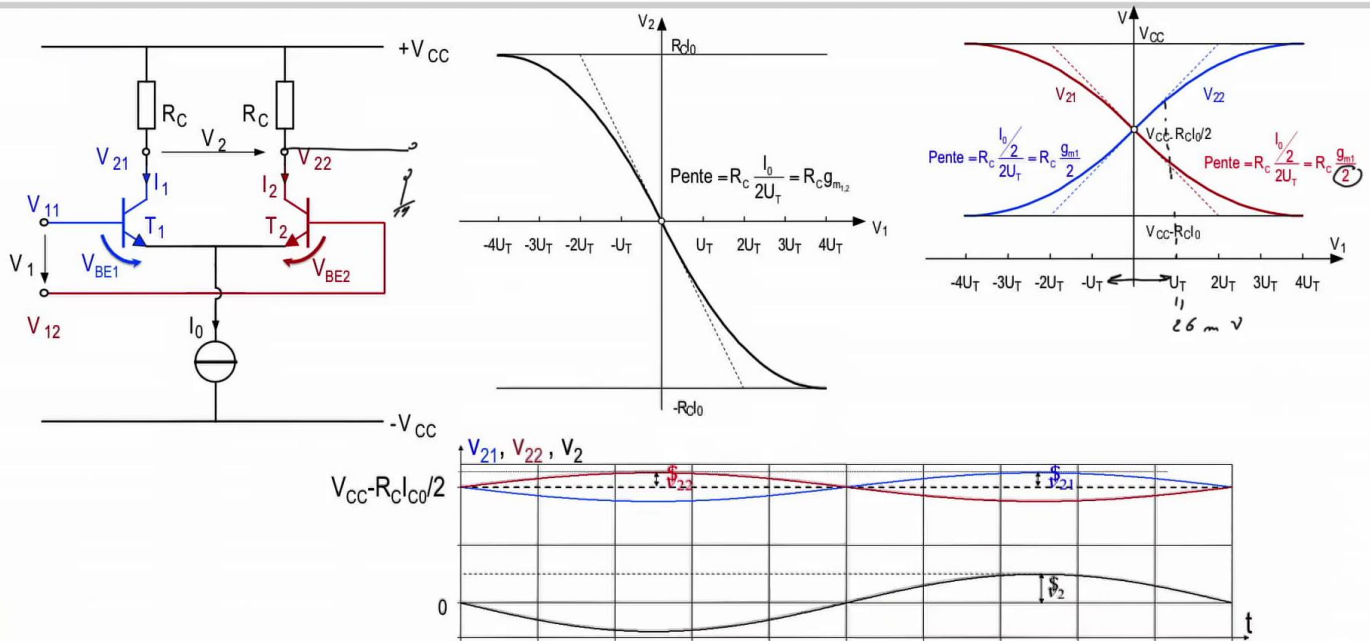
So if you are interested to V_{22} and V_{21} , look at, V_{22} compared to any fixed potential, its variation is going to be linear, when the growth is weak. So, look, when I talk about low I talk about of $(-U_T)$ and $(+U_T)$. Therefore, there is an order of magnitude of 26 mV, there is very little variation before you get anyway in the non-linearity of this curve. So we're talking about all the very small variations at the input, an increase, and this increase translates into a voltage variation at the output. But which of these tensions? It may be that tension one when I increase V_1 , I will have V_{22} to follow, it depends if I look here and there, and V_{21} which will follow from the other side. With a different terminal, this phase is positive, that phase is negative. But then, I can well look at the difference $V_{21} - V_{22}$ and then I look at that potential compared to this potential. It's exactly the swing story that we talked about, if you are on these swings, one side, it goes up, and we look at the person in front we see that we have twice of our variation, same, we see the double of the variation when one is interested in us compared to the one who move in front or, if you look directly V_{22} , with respect to a fixed potential, well, you look at the ground it is as if you are watching your swing compared to the earth so you see that you type on a fixed potential.

Notes

Summary



Caractéristiques grands signaux



Electronique II

But if you look at the person in front, which goes up and down, you will find that it's twice the dynamics. So V_2 it's taking these two curves and do the subtraction, which gives you this curve here. That is the voltage $V_2 = f(V_1)$ this is a differential voltage compared to a differential voltage it is called "differential output" "differential input". When we look at either one side or the other side, we're talking about "unilateral" or "asymmetrical" because we look compared to the ground. On this curve there, we find that the gain, it's like a transistor since the transconductance we had seen it is $(g_m / 2) \times R_C$ and on this curve one, when I look at the one in front, it is multiplied by 2 so the factor 2 which was there, seen here disappear because it is g_{m1} or g_{m2} since it is the same g_m given that the currents through the two at rest are the same. So the slope here in differential output is equal to $R_C \times g_{m1}$ so I won a factor 2 on the gain. I repeat what I just said, when I go out to one side or from each other, I designed it here with V_{21} and V_{22} admitting that I have a voltage V_1 sinusoidal at the entrance, then I see a phase is opposite to the other when the red voltage increases the other come down, and vice versa, and the peak values V_{22} and V_{21} are known on both sides are the same.

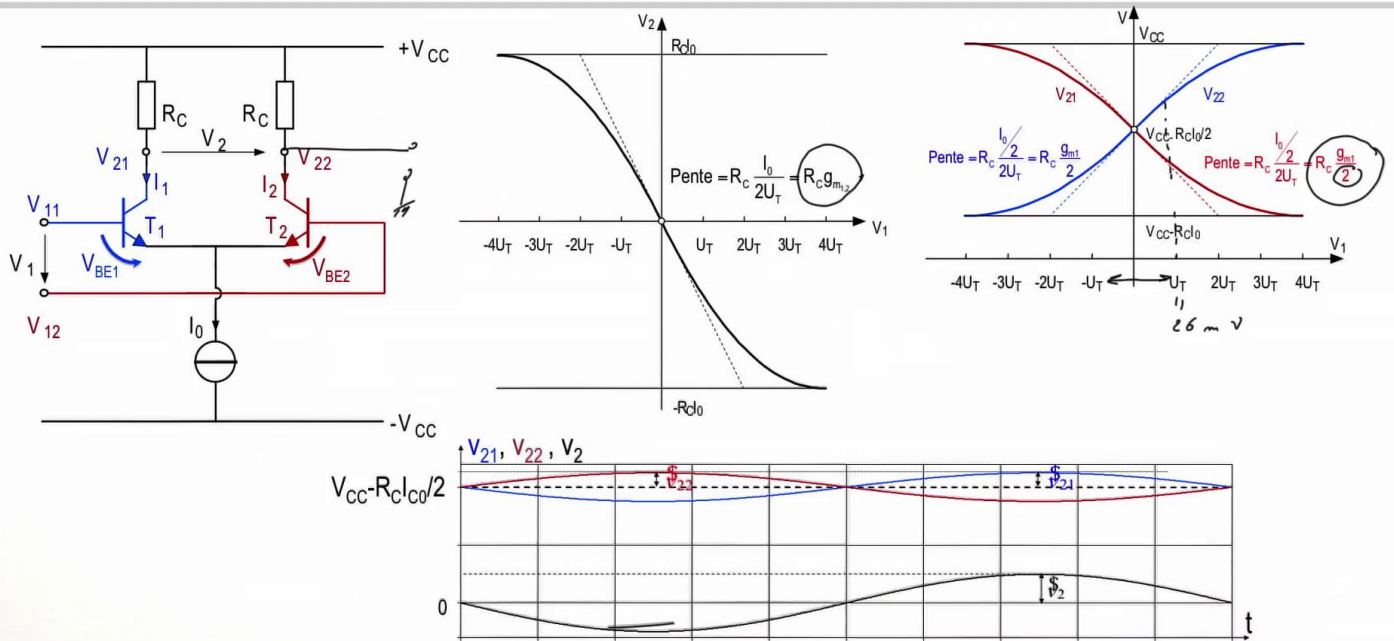
Notes

Summary



19m 27s

Caractéristiques grands signaux



Electronique II

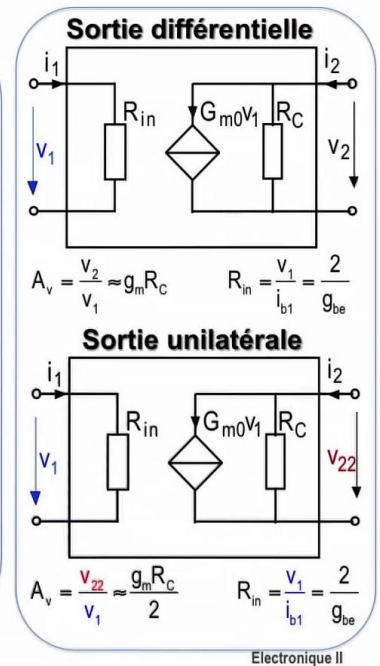
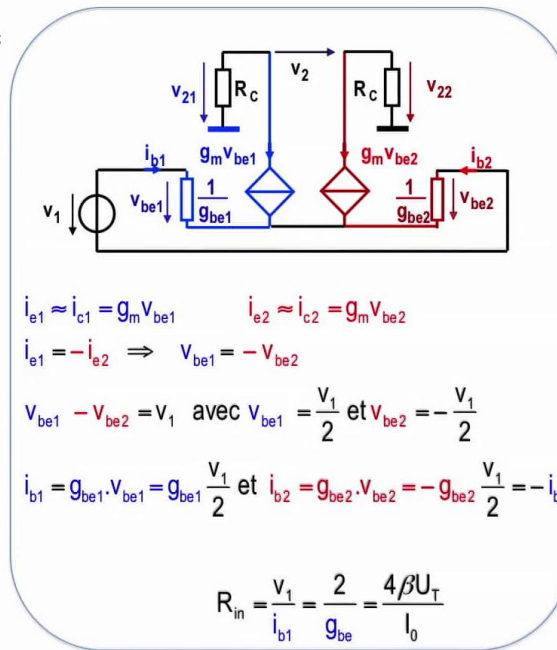
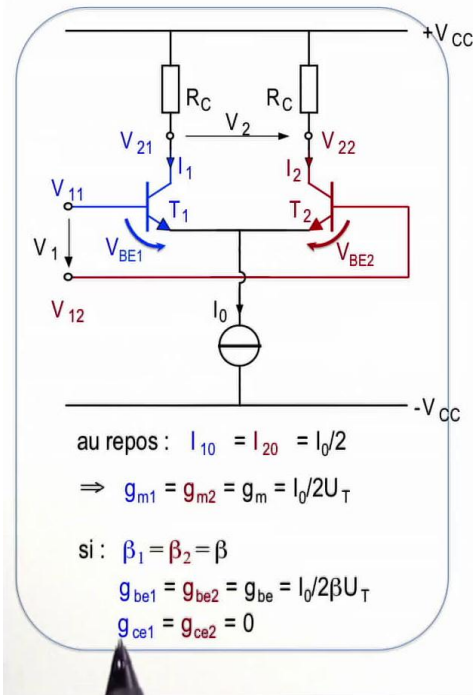
Now, if you take from that side, the difference between the two, and there you have to impose a common mode because there is not a DC potential that we look to know the common mode, this, you study it in other courses Where it is shown that by imposing common modes, in the case of resistans, there is no problem, because we switch compared to a DC potential known but we will see just now with the active loads, it will be something else. And we see a variation in tension that is double what we would have seen on one side or the other. And I will take you to remember this: the gain, when in differential output, it's like a common transmitter, the gain when we are with a unilateral release, is half of a normal common transmitter gain.

Notes

Summary



Caractéristiques petits signaux



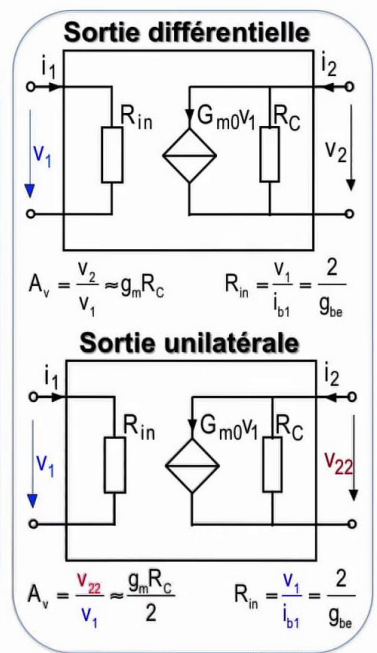
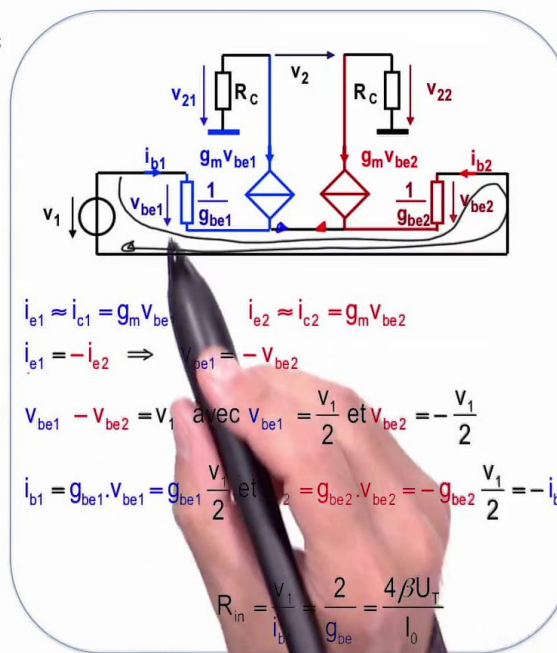
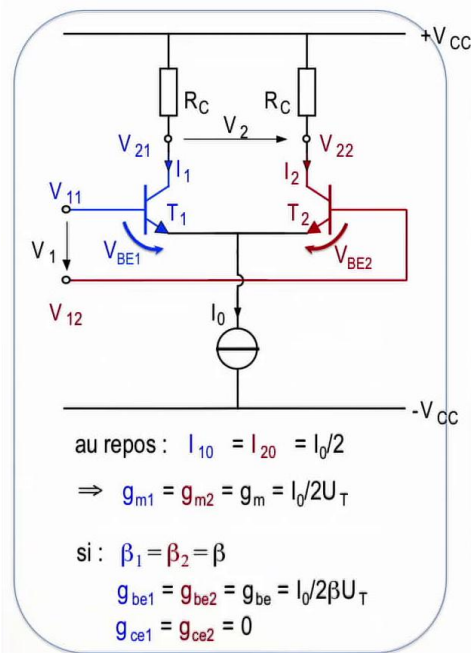
We always used to go through the scheme small signals. So we will make the scheme small signals of the differential pair. I've always presented that like that, one part with the actual pattern, that we would have achieved we draw the diagram small signal next considering that we polarized it and we extracted small signal parameters, and once we have finished it, we standardized this to replace the scheme small signals by a quadripole having an input impedance an output impedance, and a controlled current source. So we will do the same. the polarization is by this current source. As soon as the current I0 imposed here, each of the transistors, when the two voltages are the same, sees half of the current pass through. So I can write transconductances gm1 and gm2 that I call gm because it's the same thing, which in this case is equal to the polarization divided by UT therefore I0 / 2UT. Now the beta of transistors, I consider that it is the same beta. the Gbe of the transistors are the same, and it is easy to write because I know gm/beta so I divided it by beta and I find the transistor gbe and for me to be easy to do the calculation, I consider that there is no Early effect, that it is an ideal current source, the transistor T1 and T2, therefore the output conductance is equal to 0 or the output resistance of the transistors is infinite.

Notes

Summary



Caractéristiques petits signaux



And there I draw the scheme small signals. You see your transistor in blue, and your transistor in red it is a controlled current source with its RC load and look at here, as the transmitter is floating, so I put a current source it is a potential which can take any value. If it is not imposed by these two terminals, it can take any value between (+ VCC) and (- VCC). So I make this link there is a current source so it is infinite resistance I don't show it I replace, and I finally show the two input impedances. And I leave in an extremely simple reasoning. The current i_{e1} , it's the current flowing, here it is the current flowing through the transmitter there. The i_{e2} current is the current that passes through there, So it's the current that will come in this transmitter, there. The both will join but since this current and this current are in the same wire in an AC signal, thus the current $i_{e1} = -i_{e2}$. Similar to what was said to v_1 , the voltage v_1 , it appears here, like this, really like this in this mesh. So it's nothing but $V_{BE1} - V_{BE2}$. And $V_{BE1} - V_{BE2}$ is v_1 of course that's what I just wrote. When I see a voltage increase and the other decrease in the same way, it means that the voltage V_{BE1} is $v_1/2$ and V_{BE2} is $-v_1/2$.

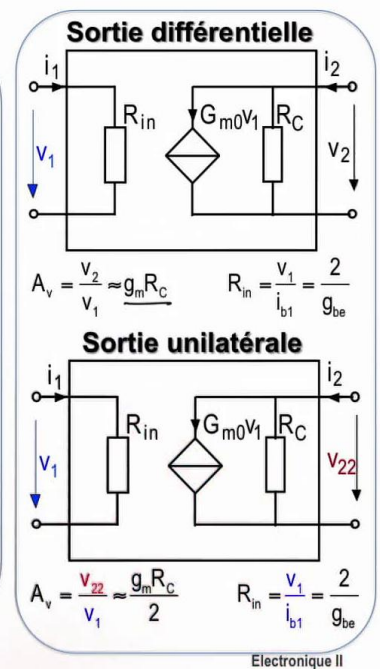
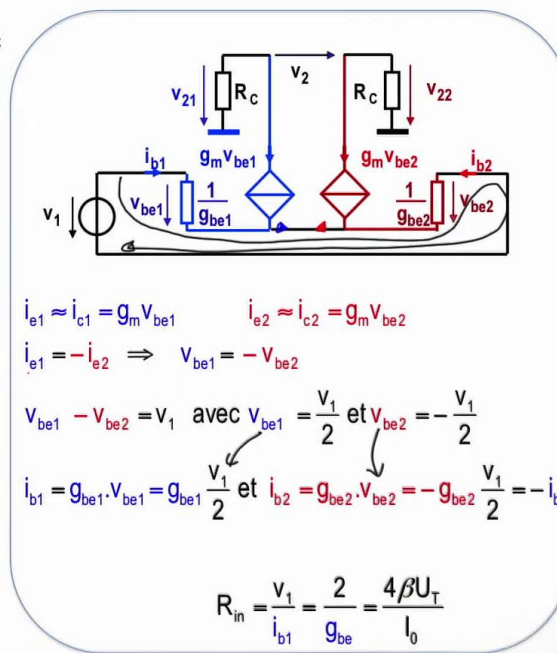
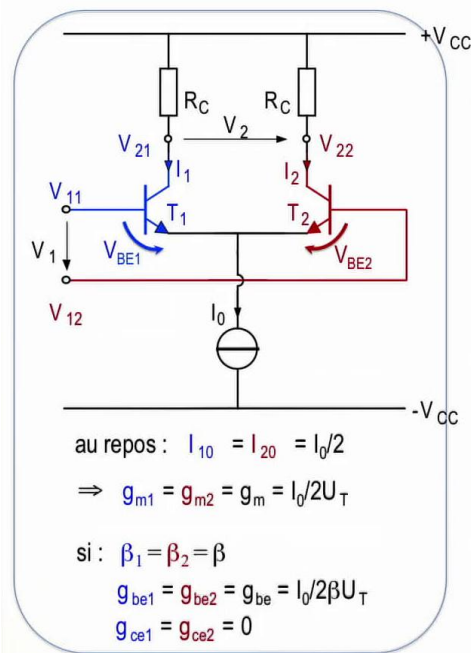
Notes

Summary



23m 17s

Caractéristiques petits signaux



So that's pretty trivial to what has been written here, and then I'm leaving in the IB1 expression, the current flowing here this is multiplied by the GBE1 VBE1, the same as what we did all the time same here, ibe2, I can write that way in red, and I can replace VBE1 by its value there and Vbe2 by its value here and it will give me this relation which easily allows me to conclude that the input impedance I see at the entrance of a differential pair which must consider the dV1 voltage or v1 divided by the IB1 current, is just 2 x (1/gbe) I remind you that for a common transmitter, it was just 1/gbe, there, I have an input resistance which is twice superior than what I would have found with a common transmitter and we can understand very well because we must provide a current to the two transistors which are connected in that way. So now I have everything I need. We earlier calculated the Gm0. It has been discovered that there are two ways: either we go out in differential, it is the ratio of this voltage, divided by this tension one. And there, it's exactly like a common transmitter, the gain is gm x RC. Why there is no sign (-)? Because it's for you to decide.

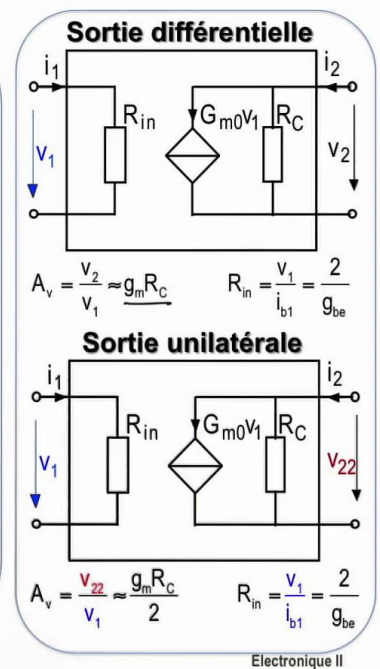
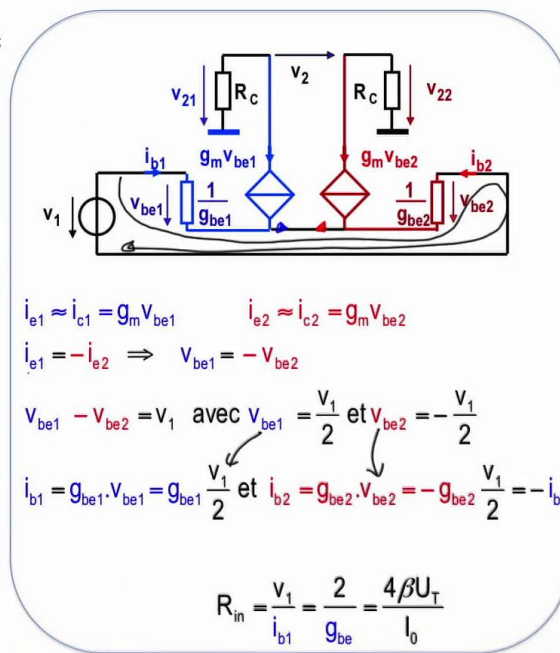
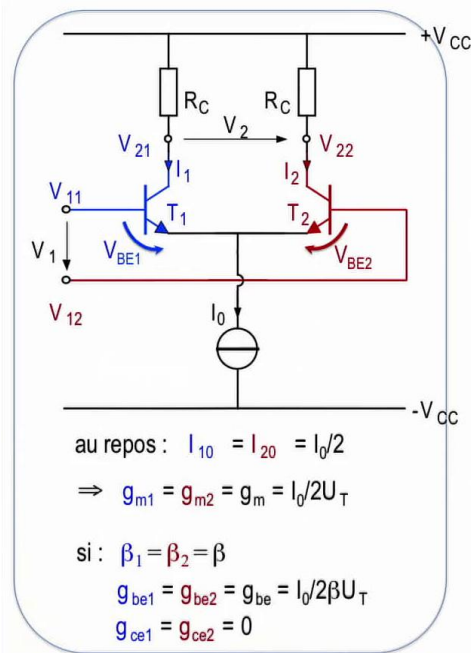
Notes

Summary



24m 58s

Caractéristiques petits signaux



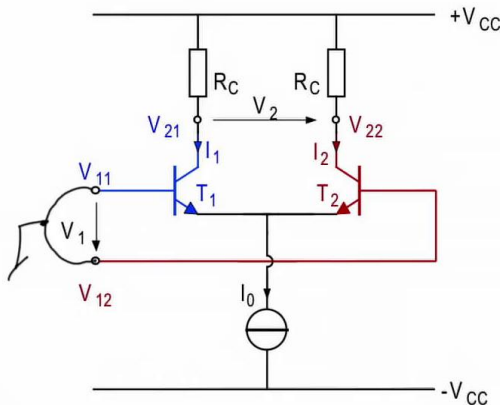
When this is differential, you can say that's positive that's negative or the contrary and then, you invert the V1 and V2 inputs. That's for you to decide where are located (+) and (-). Is it a story of terminal between V1 and V2. So the sign (-) it is added or not depending on if you decide V2, this is positive in that sense or V2 is positive in the other direction. The input impedance, is twice of a common transmitter when we have a differential input it's like a common transmitter with a difference here. Now, if I take a unilateral output, So I go out either that side either that side there, So, I forget half, it is as if I have a current I2 I operate, and the other, its variation, I let it slip in the supply I do not use it. So I lose half of effectiveness. I acted on the voltage but I have not consider the current when I go out unilaterally. So I lose half of the gain. Look at $g_m \times R_C$, and there is $g_m \times R_C/2$. And the input impedance remains the same, it does not change, it depends on the terminal one which is unaffected by the unilateral or differential output. So finally, adding these two quadrupoles which represent the differential pair in a circuit according to what comes out, either there, or on one side or the other.

Notes

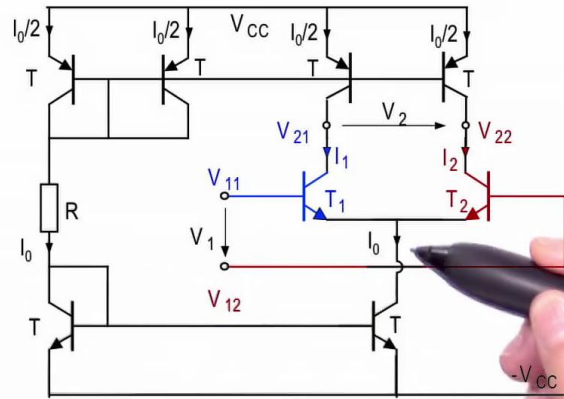
Summary



Amplificateur différentiel avec charge active



Charge passive



Charge active

And to continue in the same reasoning, a differential amplifier with active load, you remember when we took the passive loads with resistors, and we said: we do with it that we have just analyzed, passives loads and what will happen if we replace the resistances by transistors which correspond to current sources and they are currents sources that are polarized to a fixed potential and we put an active load? So that's the plan. I simply draw your attention when you take this current I_0 and connecting these two sets here, and you put a DC potential which is common between the two, well, what happen is that your current it splits, If everything is perfect, it is divided into 2 alone. Here, if you put an active load, you must be sure the current flowing there, there, added once passed by the transistor we give the current I_0 here. Otherwise, this is the origin of a systematic offset which will appear in your amplifier when all the time we have a little more current, a little less current which gives a voltage which is also balanced. So I leave you look at this diagram there. I took the power source and I realized by a current mirror to create the current I_0 .

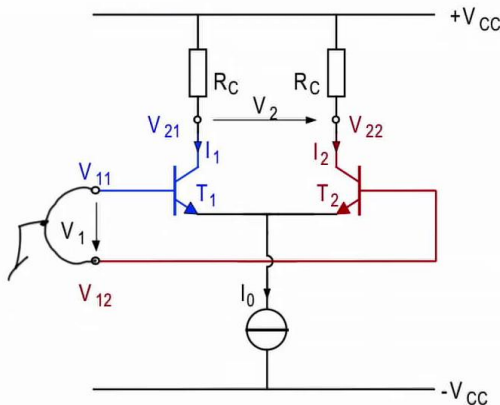
Notes

Summary

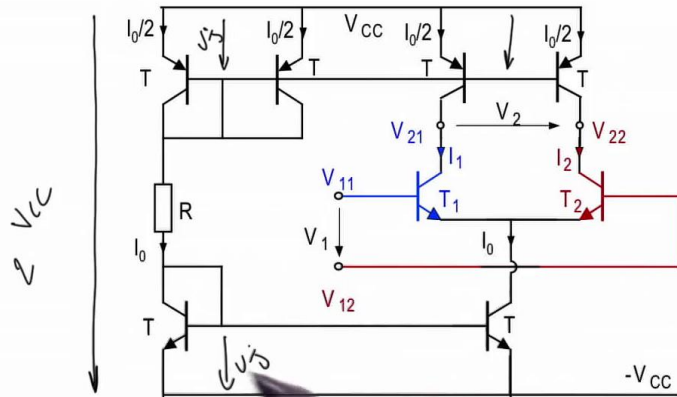


27m 51s

Amplificateur différentiel avec charge active



Charge passive



Charge active

$$I_0 = \frac{2V_{CC} - 2V_{Uj}}{R}$$

Electronique II

I use the power supply (+ VCC) (-VCC) So from here to there, I have 2 x VCC. I connect a diode connector transistor, but I put two in parallel, you'll see why, so here I have a voltage of the order of U_j and there I have a voltage of the order of U_j So I can very well calculate the current I_0 as the current I_0 , it will be easily calculated, $I_0 = 2V_{DC} - 2U_j$, therefore, it is $U_i + U_j$ and the $2V_{DC}$ due to this tension, divided by a resistor I would have chosen myself. This tension one, I know it, that tension one, I know her, I only have to determine the resistance R to impose I_0 . I come now to the active load part, I'd like two current sources, look, it's a current source it's a current source. Why? Because the voltage here is the same. There I have the same voltage as you see here. This line is connected, therefore, I have a voltage that is imposed by these two transistors. When I take the I_0 current and I make it go through two transistors absolutely the same So that structure is put into an integrated circuit, you can not do it with discrete components, you absolutely must take an integrated circuit, this tension then imposed at the base of these two transistors will absolutely copy the $I_0/2$ current in each of these two transistors.

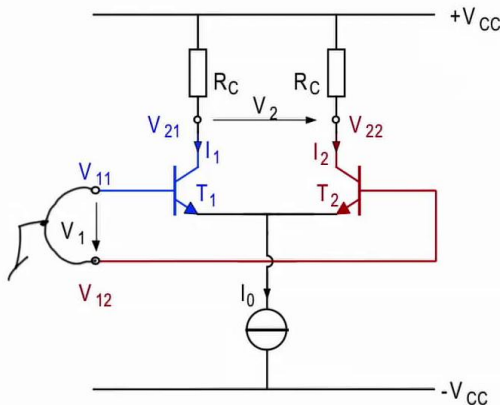
Notes

Summary

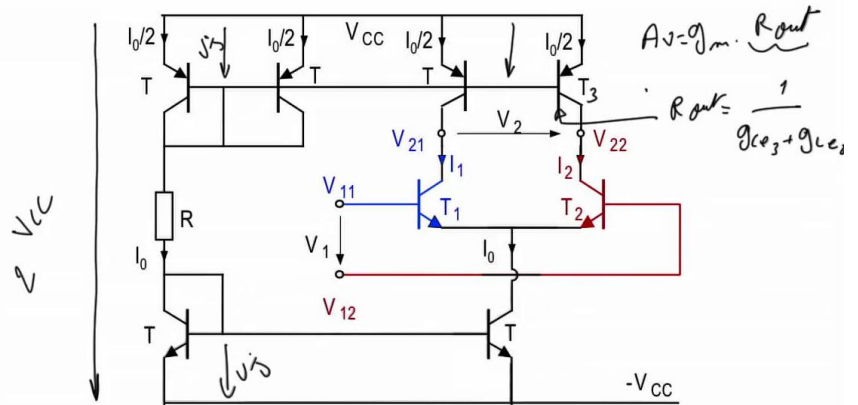


29m 19s

Amplificateur différentiel avec charge active



Charge passive



Charge active

$$I_0 = \frac{2V_{cc} - 2V_j}{R}$$

Electronique II

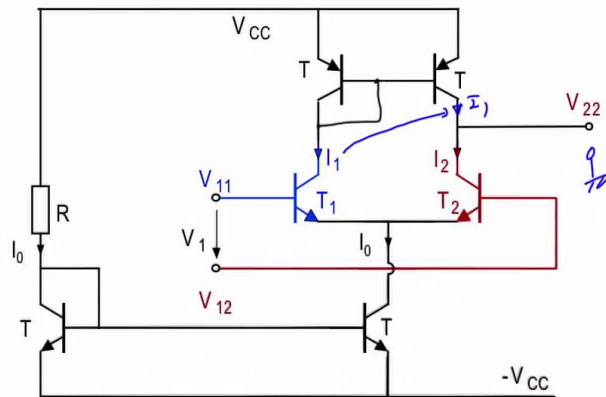
You will end up with $I_0 / 2 + I_0 / 2$ which sum up here and give you I_0 . So this structure you see here this is your differential pair we have here but brought to a structure with active load and we are left with a differential voltage and an extremely high gain because it is g_m , the gain, it is always $g_m \times R_{out}$ and this R_{out} here is huge. The resistance that I see from here R_{out} , is the parallel of $1/g_{ce}$ of this transistor in parallel with the $1/g_{ce}$ of this transistor that give you, I look at this, $1/(g_{ce3} + g_{ce2})$, we will call it 3 same on the other side. So if you multiply g_m on this gain, this output resistance, you will see that it give a gain which is phenomenal, it depends on your polarization of course, but we would have an exercise to do around it.

Notes

Summary



Amplificateur différentiel avec charge active



Electronique II

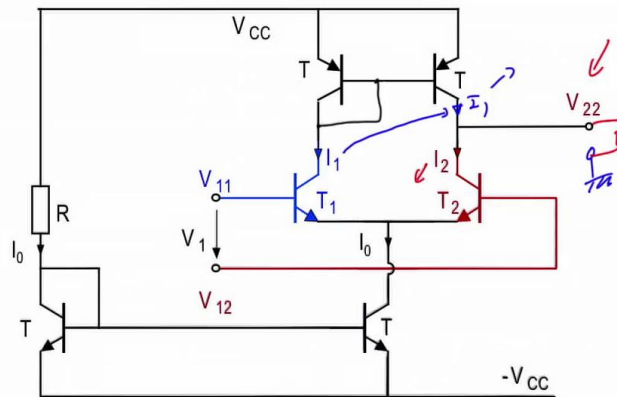
I would like to remind you what I lost just now when this link one did not exist. See this link, I'll delete it, I will delete this link then, It's like it does not exist. all the time, I just do something like that. If I polarizes the base of this transistor, of course, this arrangement would not work I would have to put a polarization what I had done in the scheme that was before. Now if I connect this, I connect there to there, there, there is another thing, it's like I tell the current I1 I'll copy it from here to there. This is a current mirror look it well, the current I1 will be here. Earlier, I had made a remark, I was said when a differential setup in which I only use half ie I have looked through what happens to that side according to that side, I just looked out, as it is now, according to a given DC potential, the variation of this current one, I left it spin in the supply and I did not use it There, in this kind of installation, It is'nt so. I take this current I1 and I sparkle it and I bring it back to the other side. I don't lose it, I do not let it go, I copied it on the other side.

Notes

Summary



Amplificateur différentiel avec charge active



$$A_v = \frac{g_m \cdot R_{out}}{2}$$

Electronique II

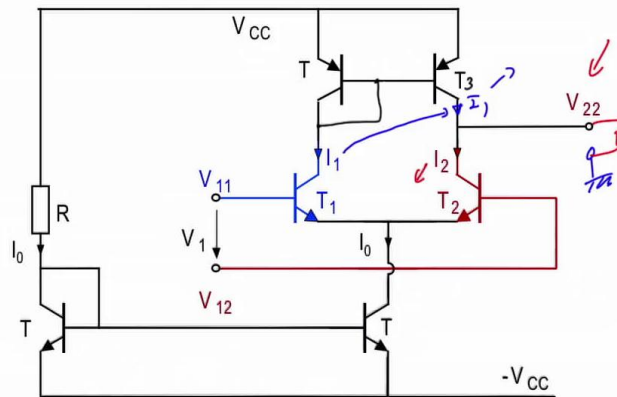
So when I_1 increases here it is expected that I_2 decreases. Yes it's right, this is what will happen, but instead of leaving this variation outside the interest of the load, if you put a load here, there you see I_1 that descends into your load and I_2 which is withdrawing from your load it corresponds to a unilateral output because I go to one side in which I no longer have a gain that was divided by 2. We were saying, unfortunately, an unilateral exit makes us lose, gives us a gain equal g_m multiplied by a load resistance, or an output resistance divided by 2. And here, in this case, since I recovered what I lost and I brought it back here, that factor 2 has been erased. So this is a setup in which I have a unilateral output and I have an absolutely full gain as a normal common emitter which is equal to $g_m \times R_{out}$ and as R_{out} remains what we have calculated earlier, which is very large, so I will find with that a gain g_m , I'll call it again transistor T_3 , it will give me back a gain $A_v = g_m / (+g_{ce3} g_{ce2})$ which is very large, I let you do the math I'll still do it quickly for you the g_m is the polarized current which passes through both, so it was said that the g_m it is a current $I_0/2$ divided by U_T .

Notes

Summary



Amplificateur différentiel avec charge active



$$A_v = \frac{g_m \cdot R_{out}}{2}$$

$$A_v = \frac{g_m}{g_{ce1} + g_{ce2}}$$

$$A_v = \frac{\frac{I_0/2}{U_T}}{\frac{I_0/2}{U_A} + \frac{I_0/2}{U_A}}$$

Electronique II

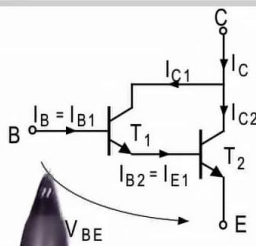
I divide, let's say both g_{ce} are the same, this transistor and this transistor have the same g_{ce2} . The two are traversed by half the current divided by the Early voltage, plus $I_0/2$, divided by the Early voltage, and I can simplify. So we see that it is independent of the current and I find myself with $2U_A / U_T$ so it will depend on the value of U_A . So that gain there, the gain of such a setup, depends on the value of the Early voltage. You can have an extremely high gain if you have low power transistors where the Early voltage is very large.

Notes

Summary



Montage Darlington et pseudo-Darlington



$$I_C = I_{C1} + I_{C2} = \beta_1 I_{B1} + \beta_2 I_{B2}$$

$$I_{B2} = I_{E1} = (\beta_1 + 1) I_{B1} = (\beta_1 + 1) I_B$$

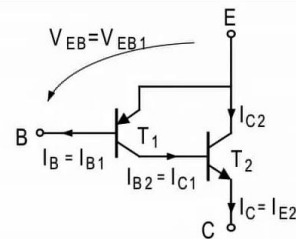
$$I_C = (\beta_1 + \beta_2 + \beta_1 \beta_2) I_B$$

$$\beta = \beta_1 + \beta_2 + \beta_1 \beta_2 \approx \beta_1 \beta_2$$

$$g_m = \frac{I_C}{V_{T2}} \approx \frac{g_{m2}}{2}$$

$$g_{be} = \frac{I_{C1}}{V_{be}} \approx \frac{I_C}{\beta_1 \beta_2 V_{be}} = \frac{g_m}{\beta_1 \beta_2} = \frac{g_{be2}}{2 \beta_1}$$

$$g_{ce} \approx g_{ce2} \approx \frac{I_{C0}}{V_A}$$



$$I_C = I_{E2} = (\beta_1 + 1) I_{B2} = (\beta_1 + 1) I_{C1}$$

$$I_{C1} = \beta_1 I_B$$

$$I_C = (\beta_2 + \beta_1 \beta_2) I_B$$

$$\beta = \beta_2 + \beta_1 \beta_2 \approx \beta_1 \beta_2$$

$$g_m = \frac{I_C}{V_{be}} \approx g_{m2}$$

$$g_{be} = \frac{I_{C1}}{V_{be}} \approx \frac{g_{be2}}{\beta_1}$$

$$g_{ce} \approx g_{ce2} \approx \frac{I_{C0}}{V_A}$$

Electronique II

I end with a setup it looks like it's just a substitution of bipolar transistors. I would like to explain the futility of this transistor. When you take a simple transistor, it has a beta, beta, you can not change it, it is in your transistor, this is one of your transistor design parameters. Now, if you take a power transistor, you can not make high betas. Your transistor, when it has to undergo a change in voltage, U_{CE} , very, very high, it suffers, physically speaking, of its inability to possess a high beta. What we do with it, we help it. If this transistor is the T2 transistor that has a low beta, we would put it with a second transistor that comes before and this is a transistor that often enough, are sold encapsulated both in a same box and it's called the Darlington circuit. So in other words, the imperfection of the transistor which has a low beta is corrected by the fact of using two transistors. And we do not forget that there I joined. There, to order it, I need 2 connections. Then I will analyze this setup and it will look like all this is calculated. I will analyze this setup taking the Darlington setup and watching what happens as if it had been a simple transistor So I say base-transmitter-collector knowing it, there are still two transistors that follow.

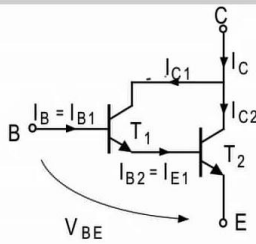
Notes

Summary



35m 48s

Montage Darlington et pseudo-Darlington



$$I_C = I_{C1} + I_{C2} = \beta_1 I_{B1} + \beta_2 I_{B2}$$

$$I_{B2} = I_{E1} = (\beta_1 + 1) I_{B1} = (\beta_1 + 1) I_B$$

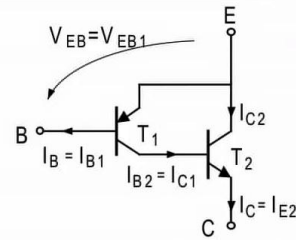
$$I_C = (\beta_1 + \beta_2 + \beta_1 \beta_2) I_B$$

$$\beta = \beta_1 + \beta_2 + \beta_1 \beta_2 \approx \beta_1 \beta_2$$

$$g_m = \frac{i_c}{v_{be}} \approx \frac{g_{m2}}{2}$$

$$g_{be} = \frac{i_b}{v_{be}} \approx \frac{i_c}{\beta_1 \beta_2 v_{be}} = \frac{g_m}{\beta_1 \beta_2} = \frac{g_{be2}}{2 \beta_1}$$

$$g_{ce} \approx g_{ce2} \approx \frac{I_{C0}}{V_A}$$



$$I_C = I_{E2} = (\beta_1 + 1) I_{B2} = (\beta_1 + 1) I_{C1}$$

$$I_{C1} = \beta_1 I_B$$

$$I_C = (\beta_2 + \beta_1 \beta_2) I_B$$

$$\beta = \beta_2 + \beta_1 \beta_2 \approx \beta_1 \beta_2$$

$$g_m = \frac{i_c}{v_{be}} \approx g_{m2}$$

$$g_{be} = \frac{i_b}{v_{be}} \approx \frac{g_{be2}}{\beta_1}$$

$$g_{ce} \approx g_{ce2} \approx \frac{I_{C0}}{V_A}$$

Electronique II

I consider that the current I_C ; that's what I wrote here, it will be divided in I_{C1} and I_{C2} here and current I_{C1} , it passes into the first transistor and it comes out the other side it becomes I_{E1} . So I can easily say that the stream that exits the I_{E1} is $\beta_1 \times I_{B1}$, and I called I_{B1} , I_B because I want at all costs to consider that there is a transistor which has 3 terminals: I_C , I_B and I_E which come in and out of this transistor. So I write this relationship as simple as it is taking I_{C1} by expressing it as being equal to I_{E1} and saying it is $\beta_1 I_{B1}$ and I calculate this and I look at what is the value of I_C when I add I_{C1} and I_{C2} including this effect because the same current of the transmitter of this transistor become the base current of this transistor T_2 . So this transistor, it will release a current here that will be its own β_2 but given that it has already taken advantage of the β_1 of this transistor that is there, therefore, it makes $\beta_1 \times \beta_2$ as an approximation of the two gains. So if you calculate that expression, You find that the current that comes out, or rather the current I_C , that's I_B multiplied by the product of the β s of the two transistors plus β_2 , plus β_1 .

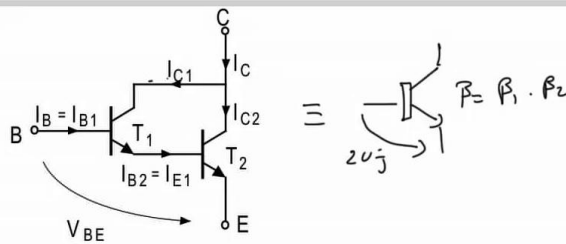
Notes

Summary



37m 31s

Montage Darlington et pseudo-Darlington



$$I_C = I_{C1} + I_{C2} = \beta_1 I_{B1} + \beta_2 I_{B2}$$

$$I_{B2} = I_{E1} = (\beta_1 + 1) I_{B1} = (\beta_1 + 1) I_B$$

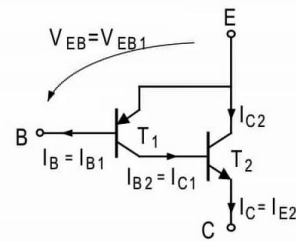
$$I_C = (\beta_1 + \beta_2 + \beta_1 \beta_2) I_B$$

$$\beta = \beta_1 + \beta_2 + \beta_1 \beta_2 \approx \beta_1 \beta_2$$

$$g_m = \frac{i_c}{v_{be}} \approx \frac{g_{m2}}{2}$$

$$g_{be} = \frac{i_b}{v_{be}} = \frac{i_c}{\beta_1 \beta_2 v_{be}} = \frac{g_m}{\beta_1 \beta_2} = \frac{g_{be2}}{2 \beta_1}$$

$$g_{ce} \approx g_{ce2} \approx \frac{I_{C0}}{V_A}$$



$$I_C = I_{E2} = (\beta_1 + 1) I_{B2} = (\beta_1 + 1) I_{C1}$$

$$I_{C1} = \beta_1 I_B$$

$$I_C = (\beta_2 + \beta_1 \beta_2) I_B$$

$$\beta = \beta_2 + \beta_1 \beta_2 \approx \beta_1 \beta_2$$

$$g_m = \frac{i_c}{v_{be}} \approx g_{m2}$$

$$g_{be} = \frac{i_b}{v_{be}} \approx \frac{g_{be2}}{\beta_1}$$

$$g_{ce} \approx g_{ce2} \approx \frac{I_{C0}}{V_A}$$

Electronique II

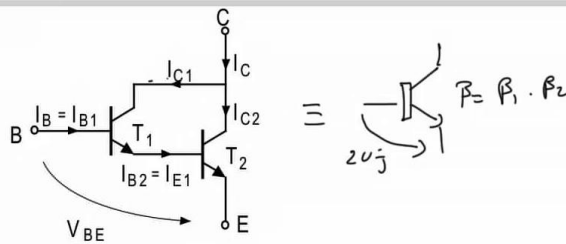
We can very well simplify $(\beta_1 + \beta_2)$ compared to the product of $(\beta_1 \beta_2)$ and say this is of the order of magnitude of $\beta_1 \times \beta_2$. So I just realized one equivalent of a transistor, if I draw bizarrely, we'll say that it is a super-transistor so the beta equals to $\beta_1 \times \beta_2$ that a manufacturer gives you, but he tells you "Caution, there you are going to have two junction voltages when you order it." Because there is 2 junctions following each other. Someone who says "I have two junction voltages, if I use it in an increase, the Voltage V_{BE} delta will be divided on two transistors, which brings a g_m on 2." You remember that the voltage variation generates a current variation, but then, this transistor instead of seeing a change, it will lose a variation on the first, which brings us roughly to say it has lost its transconductance because it needs twice variation to give us an equivalent change in current. Thus, the g_m is divided by 2. Taking this expression and saying that the g_{be} , the input impedance, it's g_m/β but the β , it became $\beta_1 \times \beta_2$, I can very well say it's $g_m / (\beta_1 \beta_2)$ I can bring to the output transistor $g_{be2} / 2\beta_1$ Early voltage is not affected because we will say to the approximation is the Early voltage of the transistor T2 will dominate because there is an Early voltage here but it does not bother us to see the output.

Notes

Summary



Montage Darlington et pseudo-Darlington



$$I_C = I_{C1} + I_{C2} = \beta_1 I_{B1} + \beta_2 I_{B2}$$

$$I_{B2} = I_{E1} = (\beta_1 + 1) I_{B1} = (\beta_1 + 1) I_B$$

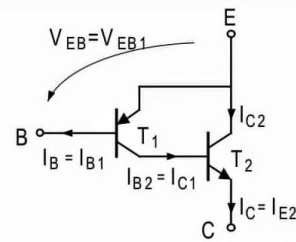
$$I_C = (\beta_1 + \beta_2 + \beta_1 \beta_2) I_B$$

$$\beta = \beta_1 + \beta_2 + \beta_1 \beta_2 \approx \beta_1 \beta_2$$

$$g_m = \frac{i_c}{v_{be}} \approx \frac{g_{m2}}{2}$$

$$g_{be} = \frac{i_b}{v_{be}} \approx \frac{i_c}{\beta_1 \beta_2 v_{be}} = \frac{g_m}{\beta_1 \beta_2} = \frac{g_{be2}}{2 \beta_1}$$

$$g_{ce} \approx g_{ce2} \approx \frac{I_{C0}}{V_A}$$



$$I_C = I_{E2} = (\beta_1 + 1) I_{B2} = (\beta_1 + 1) I_{C1}$$

$$I_{C1} = \beta_1 I_B$$

$$I_C = (\beta_2 + \beta_1 \beta_2) I_B$$

$$\beta = \beta_2 + \beta_1 \beta_2 \approx \beta_1 \beta_2$$

$$g_m = \frac{i_c}{v_{be}} \approx g_{m2}$$

$$g_{be} = \frac{i_b}{v_{be}} \approx \frac{g_{be2}}{\beta_1}$$

$$g_{ce} \approx g_{ce2} \approx \frac{I_{C0}}{V_A}$$

Electronique II

So I find these expressions and there is an setup so-called Darlington because we used two transistor of the same type and NPN and NPN I can do of course with PNP and PNP. But if I mix the transistors, one PNP, one NPN, in the PNP one, this is the control transistor, this is the one that will see the variation between the base and transmitter and the NPN transistor, this is the one that will play the output interface, I'll see there, what I have gained according to this, is that the gm wich was divided by 2 because of the fact that I lost twice the junction voltage when ordering, then I took it back to a junction voltage. So that will bring me to a transconductance as transconductance of a normal transistor. I won on transconductance and then, in terms of beta, I fall back on the same thing, more or less, beta1 beta2 x as a proxy. Now, what will happen with the input impedance?

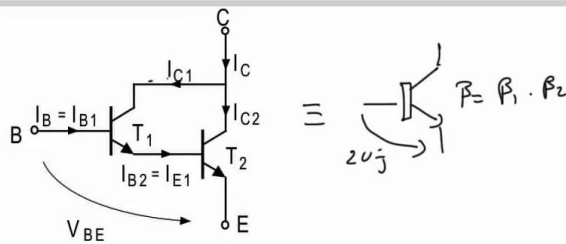
Notes

Summary



40m 31s

Montage Darlington et pseudo-Darlington



$$I_C = I_{C1} + I_{C2} = \beta_1 I_{B1} + \beta_2 I_{B2}$$

$$I_{B2} = I_{E1} = (\beta_1 + 1) I_{B1} = (\beta_1 + 1) I_B$$

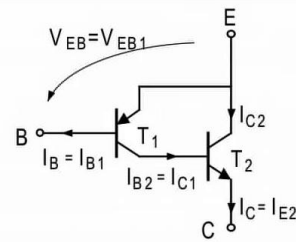
$$I_C = (\beta_1 + \beta_2 + \beta_1 \beta_2) I_B$$

$$\beta = \beta_1 + \beta_2 + \beta_1 \beta_2 \approx \beta_1 \beta_2$$

$$g_m = \frac{i_c}{v_{be}} \approx \frac{g_{m2}}{2}$$

$$g_{be} = \frac{i_b}{v_{be}} \approx \frac{i_c}{\beta_1 \beta_2 v_{be}} = \frac{g_m}{\beta_1 \beta_2} = \frac{g_{be2}}{2 \beta_1}$$

$$g_{ce} \approx g_{ce2} \approx \frac{I_{C0}}{V_A}$$



$$I_C = I_{E2} = (\beta_1 + 1) I_{B2} = (\beta_1 + 1) I_{C1}$$

$$I_{C1} = \beta_1 I_B$$

$$I_C = (\beta_2 + \beta_1 \beta_2) I_B$$

$$\beta = \beta_2 + \beta_1 \beta_2 \approx \beta_1 \beta_2$$

$$g_m = \frac{i_c}{v_{be}} \approx g_{m2}$$

$$g_{be} = \frac{i_b}{v_{be}} \approx \frac{g_{be2}}{\beta_1}$$

$$g_{ce} \approx g_{ce2} \approx \frac{I_{C0}}{V_A}$$

Electronique II

The value of the input impedance here is not the same as there simply because the g_{m2} there was $g_{m2}/2$ which made me gain a factor of 2 on the input resistance, the input resistance is $2\beta_1 / g_{m2}$, then it will become g_{m2} / β_1 . So, I have the factor 2 which is missing here, therefore the input resistance of a setup made by a pseudo-Darlington, allows me to improve the gain setting which is the transconductance and it allows me to lose a factor of 2 on the input resistance, there, the input resistor is two times higher than what I have seen here while the output impedance is the same, the g_{ce} is the same. I have just finished a completely new structure, the differential setup which closed the series of analog structures that we will use to do with amplifiers and mostly transconductances. And it is one of the transconductances that is the most used, in this case, the input of an operational amplifier uses an input (+) and (-), so this is a differential pair and therefore this part of my course, ended, with just a variety of a bipolar transistor who was to booster the beta through the use of two transistors to multiply the beta and obtain a product of betas between two transistors.

Notes

Summary



41m 35s